



Enhancement of Photovoltaic Pressurized Irrigation System Based on Hybrid Kalman Fuzzy

Suwito Suwito¹Mochamad Ashari^{1*}Muhammad Rivai¹M. Anis Mustaghfirin²

¹*Department of Electrical Engineering, Institut Teknologi Sepuluh Nopember, Indonesia*

²*Department of Marine Engineering, Politeknik Perkapalan Negeri Surabaya, Indonesia*

* Corresponding author's Email: ashari@ee.its.ac.id

Abstract: This paper presents an enhancement of a pressurized irrigation system without battery and water tank storage. The system is powered by a photovoltaic (PV) system with a hybrid Kalman filter and fuzzy logic (HKF)-based control system. The Kalman filter estimates the maximum power point, whereas fuzzy logic controls the boost converter to optimize the PV output. The system manages the water pressure by matching the power of the brushless DC (BLDC) motor and the number of valves to be operated. A prototype of the system was built on a laboratory scale using a 32-bit ARM microcontroller and pressurized irrigation networks. Results from the simulation and prototype tests were very similar in terms of tracking the optimum power. The average steady-state oscillation amplitude is 0.65 watts, while the average rise time is 1.02 seconds. The performance of the HKF is much better than perturb and observe (P&O) method.

Keywords: Fuzzy logic, Pressurized irrigation, Kalman filter, Microcontroller, Maximum power point tracking, Photovoltaic.

1. Introduction

The utilization of PV panels as a source of energy for irrigation in remote agricultural land is gaining popularity [1, 2]. Increasingly expensive national electricity prices and cheaper PV panel prices encourage PV as an energy source in the agricultural irrigation sector [3-5]. The solar photovoltaic pressurized irrigation system (SPVPIS) is the most efficient type of irrigation for electricity and water consumption. This irrigation system distributes water from the underground tank, pumped directly through the irrigation pipe network to the plants with slight discharge and volume according to the plant's needs. The consistent emitter discharge, which is impacted by the irrigation operating pressure (IOP), is one of the effective variables in ensuring the intended performance of the pressurized irrigation system [6].

SPVPIS without energy storage is preferred because it is cheaper, and there are no investment or maintenance costs for the energy storage [7, 8]. Although SPVPIS is the most efficient, it is

susceptible to solar irradiation because it must be used simultaneously when generated [7]. Therefore, the success of this system depends on the controller's ability to optimize and instantly manage the available PV energy to meet the demand. Maximum power point tracking (MPPT) is the most efficient way to optimize PV energy. The basic principle of MPPT is to adjust the PV load impedance until the maximum power point (MPP) is obtained [9, 10].

Many researchers have studied the optimization of PV-powered irrigation systems. Several researchers developed the MPPT method without using a DC converter but by controlling the speed of a BLDC motor-driven pump. The technique they developed aims to reduce the cost and energy loss due to the DC converter [11]. Although the power losses can be reduced, direct MPPT control through the BLDC motor drive inverter causes the MPPT response to be slow and produces quite large oscillations in the MPP. Other researchers have developed MPPT using Cuk [12], Landsman [13], and Zeta DC converters which are controlled by the

NOMENCLATURE**PV Generation Side**

P_{mpp}	Power at maximum power
V_{mpp}	Voltage at maximum power
I_{mpp}	Current at maximum power
V_{OC}	Open-circuit voltage of the PV
I_{SC}	Short-circuit current of the PV
I	Output current of the PV cell
I_{ph}	Photocurrent of the PV cell
I_o	Saturation current of PV cell
q	Electron charge ($1.6 \times 10^{-19}C$)
V_d	Voltage imposed across the cell
K_t	Temp. Coeff. of cell's short circuit current
K	Boltzmann's constant ($1.38 \times 10^{-23} J/K$)
T	PV cell temperature
T_{ref}	PV reference temperature (298^0K)
β	Irradiation intensity
n	Ideal factor (1.7)

BLDC Motor Side

ω	Angular speed of the motor
T_m	Electromagnetic torque
e_a	Back-EMF in phase a
i_a	Current per phase a
η_m	BLDC motor efficiency

Boost Converter Side

V_{in}	Input voltage on the boost converter.
V_{out}	Output voltage on the boost converter.
D	Duty cycle of boost converter
f_{sw}	Switching frequency of the converter

Pressurized Irrigation Side

P_{whp}	Water horsepower
ρ	Density of water (1000 kg/m^3)
g	Gravitational constant (9.8 m/s^2)
H_p	Total pump head
Q_p	Pump discharge
η_p	Water pump efficiency

Hybrid Kalman-Fuzzy Method Side

\hat{V}_k^-	Predicted V_{mpp} in k^{th} iterations
P_k^-	Priori error covariance in k^{th} iterations
K_k	Kalman gain in k^{th} iterations
\hat{V}_k	Updated estimate of the V_{mpp} in k^{th} iterations
P_k	Update error covariance in k^{th} iterations
Q	Process noise covariance
R	Measurement noise covariance
M	Scaling factor
$P_{pv,k}$	PV output voltage at k^{th} iterations
$V_{pv,k}$	PV output power at k^{th} iterations

incremental conductance (INC) method [14]. The disadvantage of conventional INC control in these studies is the relatively large oscillation in the MPP. Some researchers apply fuzzy logic controller (FLC) to photovoltaic water pump systems with a fixed hydraulic load, namely lifting water to a reservoir at a fixed height [15]. The method still has significant oscillations during the transition which causes the pump speed to oscillate. Research related to irrigation management based on sensors of soil moisture, temperature, and light intensity that is processed using FLC is able to control irrigation capacity very accurately [16]. However, because PV panels have not been used as an energy source, this method is difficult to implement in remote areas. The division of irrigation areas into several sectors, or called multi-sector, has succeeded in reducing the cost of PV generation and increasing energy efficiency [7, 17, 18]. However, the study did not pay attention to the optimization of PV output power and did not consider the irrigation dose error due to changes in IOP.

Studies related to MPPT that are applied to the solar photovoltaic water pump (SPVWP) still have problems, namely relatively slow response and power oscillations in MPP. If the system is used in SPVPIS, it will result in fluctuating IOP which will eventually lead to inaccurate water dosing. The unsynchronization between the availability of PV output power and irrigation capacity worsens the stability of the IOP.

The main objective of the proposed system is to increase the optimization of SPVPIS using MPPT, which is synchronized with the irrigation sector controller. The novelty of this research is MPPT control using Kalman filter, and (FLC called hybrid Kalman fuzzy (HKF)). Compared to the FLC method in other studies, this proposed method has a faster transient response and has lower power oscillations at MPP. The Kalman filter estimates the MPP voltage while the FLC controls the DC converter to achieve MPP based on the error voltage between the MPP voltage estimate and the actual PV voltage. The

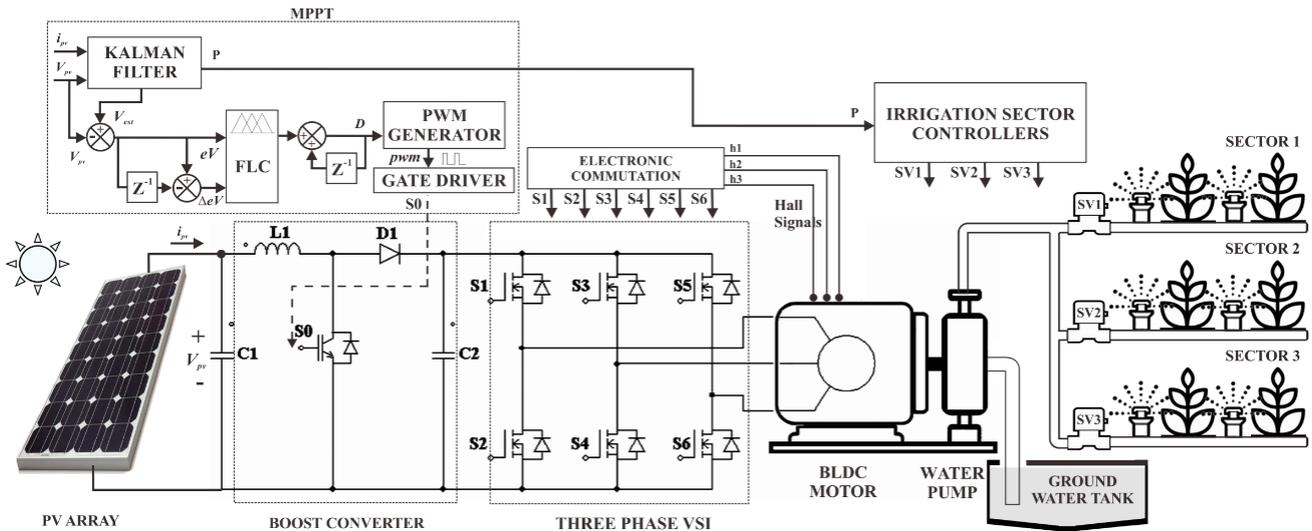


Figure. 1 The functional diagram of the proposed system

method offered has an accurate and fast MPP tracking performance and has a low steady-state oscillation. The Kalman filter has efficient computation and supports the estimation of the present, past, and future states [19, 20]. This filter can also estimate when the system's character being modeled is unknown. Efficient computing makes the Kalman filter easy to implement on a microcontroller. Fuzzy logic resembles humans and can be adapted to nonlinear control commands [21]. Fuzzy logic is also very effective in dealing with complex processes, and the mathematical model is unknown [22]. This HKF-based MPPT method has been applied to the SPVPIS prototype. The system built is simulated on MATLAB/SIMULINK and verified through experiments with hardware.

This paper is structured as follows: Section 2 describes our proposed system. A detailed discussion of the optimization and control methods is discussed in Section 3. The simulation and experimental preparation, and test results are discussed in Section 4. Section 5 presents the conclusions of this paper.

2. The proposed system

A functional diagram of the proposed system is presented in Fig. 1. The system consists of several subsystems: a PV array, a boost converter with fuzzy logic as an MPPT controller, inverter-BLDC motor, water pump set, and pressurized irrigation network with the Kalman filter controller. This system focuses on optimizing the PV output using the MPPT based on the HKF method. The PV output power is optimally used by adjusting the irrigation capacity according to the output power.

2.1 PV characteristics

The PV panels are a series and parallel combination of PV cells having the equivalent circuit shown in Fig. 2. The photovoltaic current is affected by solar irradiation and the temperature of the PV panel according to Eq. (1). The shunt resistance (R_{sh}) is typically much greater than the load resistance, whereas the series resistance (R_s) is much less. As a result of omitting these two resistances, the cell output current can be expressed as Eq. (2) [23, 24].

$$I_{ph} = [I_{sc} + K_t(T - T_{ref})] \frac{\beta}{1000 \text{ W/m}^2} \quad (1)$$

where I_{ph} , is the photovoltaic current generated by solar irradiation (A), I_{sc} is the PV short circuit current at $25^\circ\text{C} / \text{kW/m}^2$, K_t is temperature coefficient of cell's short circuit current, T_{ref} is the PV reference temperature (298°K), and β is the irradiation intensity (W/m^2).

$$I = I_{ph} - I_o [e^{qV_d/nKT} - 1] \quad (2)$$

where I is the output current of the PV cell, I_o is the saturation current of PV cell, q is the electron charge ($1.6 \times 10^{-19}\text{C}$), V_d is the voltage imposed across the

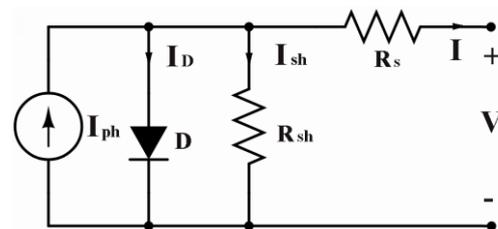


Figure. 2 PV equivalent circuit

Table 1. Specifications of the PV modules used

Characteristics	Value
Maximum power P_{mpp}	100W
Maximum Power Voltage V_{mpp}	18V
Maximum Power Current I_{mpp}	5.56A
Short-Circuit Current I_{SC}	6.00A
Open-Circuit Voltage V_{OC}	22.5V
Temperature coefficient of V_{OC}	-0.33% /°C
Temperature coefficient of I_{SC}	-0.0055% /°C

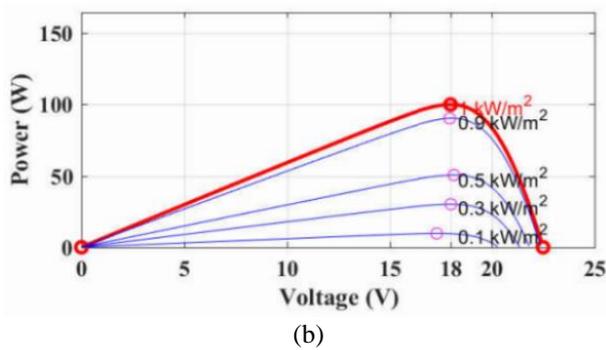
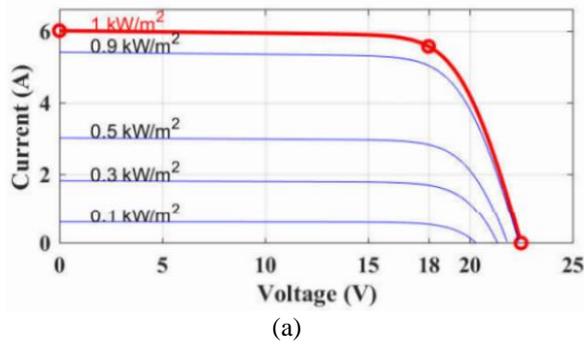


Figure. 3 PV characteristic curve, a) I-V and b) P-V

cell, n is the ideal factor (1.7), K is Boltzmann’s constant (1.38×10^{-23} J/K), T is the cell temperature (K).

This study used monocrystalline PV panels with a capacity of 100 WP. The specifications of the PV panels are presented in Table 1. The current-voltage (I-V) and power-voltage (P-V) characteristic curves are shown in Fig. 3. In this study, the PV model at the system simulation steps uses the model provided by MATLAB/SIMULINK. The parameters of the PV model are filled in according to the PV panel specification data from the manufacturer. In the experimental steps, the PV model uses a PV emulator whose irradiation value can be programmed. The PV power capacity in the simulation model and PV emulator is the same as 100Wp.

2.2 Characteristics of BLDC motor-driven water pump

Pressurized irrigation networks require a water supply at a certain pressure. Generally, this supply is

obtained from the water reservoir tank and pumped into the irrigation network. This system uses a BLDC motor-driven centrifugal pump. The BLDC motor has an equivalent circuit similar to a 3-phase synchronous motor, as shown in Fig. 1. The BLDC motor drive uses a three-phase voltage source inverter (VSI) with an electronic commutation or phase controller based on the rotor position via a Hall sensor. The method used in this electronic commutation is a six-step method. The stator current is directly proportional to the DC link voltage (V_{dc}) at the VSI [25]. The angular speed of the motor is directly proportional to the stator current, according to Eq. (3).

$$\omega_m = \frac{e_a i_a + e_b i_b + e_c i_c}{T_m} \quad (3)$$

The water pump and the BLDC motor are connected in one shaft, so the pump speed is the same as the BLDC motor speed. The characteristics of the BLDC motor used in this system are listed in Table 2. The centrifugal pump used in this study has a head-flow rate characteristic curve, as shown in Fig. 4. The maximum head (H_p) of the pump was 27 m, and the maximum flow rate (Q_p) was 80 l/m. The maximum pump efficiency was achieved when the flow rate was 50 l/m. The hydraulic power of the pump output is called the water horsepower (P_{whp}) calculated based on Eq. (4).

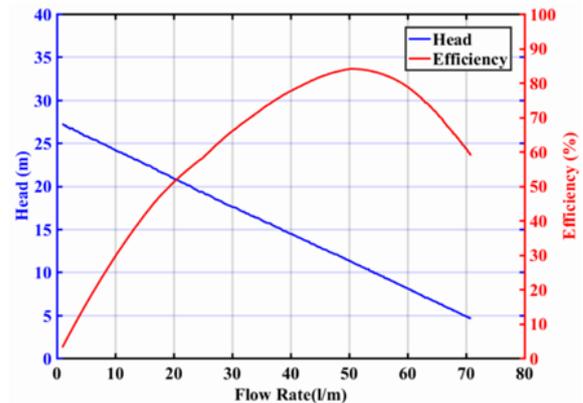


Figure. 4 Head-Capacity curve characteristic of centrifugal pump.

Table 2. BLDC motor parameters.

Parameters	Value
Rated power	125 W
Rated speed	3000 RPM
Rated voltage	24 V
Poles	4
Back EMF Constant	12 V/kRPM
Phase resistance	0.3 Ω
Phase inductance	0.00035 mH

$$P_{whp} = \rho g H_p Q_p \tag{4}$$

where, ρ is the density of water (1000 kg/m³), and g is the gravitational constant, 9.8 m/s².

The correlation between the electric power of the pump (P_{i_pump}) and P_{whp} is given by Eq. (5).

$$P_{i_pump} = \frac{P_{whp}}{\eta_m \eta_p} \tag{5}$$

where η_m is the efficiency of the BLDC motor, and η_p is the efficiency of the water pump head. The value of η_m is approximately 0.85, and η_p is approximately 0.80.

2.3 Design of the boost converter

The boost converter is an actuator of the MPPT, which functions to increase the voltage from the PV output to the load. This boost converter has the configuration shown in Fig. 1, consisting of inductor L_1 , fast recovery diode D_1 , capacitor C_2 , and MOSFET switch S_0 . The MPPT controller controls the boost converter via S_0 using a pulse width modulation (PWM) signal. The signal is representative of the calculation results of the HKF control method.

The converter output voltage V_{out} is calculated based on Eq. (6), and the converter output power P_{out} is obtained by Eq. (7). The relationship between the converter input power P_{in} and duty cycle (D) according to Eq. (8).

$$V_{out} = \frac{V_{in}}{1-D} \tag{6}$$

$$P_{out} = \frac{V_{out}^2}{R_L} = \frac{V_{in}^2}{(1-D)^2 R_L} \tag{7}$$

$$P_{in} = \frac{1}{\eta_{conv}} P_{out} = \frac{1}{\eta_{conv}} \frac{V_{in}^2}{(1-D)^2 R_L} \tag{8}$$

The parameters of the boost converter are calculated based on the equation in Table 3. The boost converter efficiency value (η_{conv}) depends on the quality of the converter components and generally ranges from 80% to 98%.

2.4 Topology of pressurized irrigation network

The proposed pressurized irrigation network comprises several outlets that supply water to a particular irrigation sector. Each outlet or lateral has several emitters from which water exits to the land. Emitter water discharge is influenced by emitter type and IOP. The relationship between the dripper discharge and IOP of the emitters according to Eq. (9) [26].

$$q_j = K_d H^x \tag{9}$$

Where q_j the discharge of dripper l/h is, K_d is the coefficient of the dripper, H is the IOP (m), and x is the exponent for the flow regime. Based on Eq. (7) shows that the relationship between IOP and emitter discharge is not linear. Therefore, in pressurized irrigation systems, it is recommended that IOP be maintained at a certain pressure. The IOP set point for this system was 8 psi or 5.63 m.

The water discharge requirement for each sector is calculated based on Eq. (10).

$$Q_j = n_j q_j \tag{10}$$

Where Q_j the flow of a specific sector (j) is, n_j is the number of emitters per sector, and q_j is the emitter discharge (l/h). The value of q_j in this system is 4 l/h with $n_j = 300$, so the value of Q_j is 1200 l/h. This irrigation network was assumed to be flat, and the emitter type was drip-line. The hydraulic capacity of each sector (P_j) in watts was calculated based on Eq. (11).

$$P_j = \rho g H_{rj} Q_j \tag{11}$$

3. The optimization and control design

The functional diagram of the HKF method is shown in Fig. 5. The estimated MPP voltage generated by the Kalman filter is compared with the actual PV voltage resulting in a voltage difference

Table 3. DC boost converter design parameters

Parameters	Expression	Data	Value
D	$D = \frac{V_{out} - V_{in}}{V_{out}}$	$V_{in} = 18$ V $V_{out} = 24$ V	0.25
L_1	$L_1 = \frac{DV_{in}}{f_{sw} \Delta I_{out}}$	$f_{sw} = 20$ kHz $I_L = 3.3$ A $\Delta I_{out} = 0.05 I_{out}$ $= 0.165$ A	1.4 mH
C_2	$\omega = \frac{2\pi N_r P}{120}$ $I_{out} = \frac{P_{mpp}}{V_{out}}$ $C = \frac{I_{out}}{6 \omega \Delta V_{out}}$	$P = 4$ $N_r = 3000$ rpm $V_{out} = 24$ V $P_{mpp} = 100$ W $\Delta V_{out} = 0.02 V_{dc}$ $= 0.6$ V	1.8 mF

called voltage error. The voltage error (VE) and the change in voltage error (ΔVE) then become input for the FLC to control the boost converter so that the PV output power reaches MPP.

3.1 Kalman filter design for MPPT

The V_{mpp} estimation process carried out by the Kalman filter proceeds in two stages. The first step is the prediction state, and the second step is the measurement update. The two steps are iterated to reduce noise, and the covariance error is zero [17]. The prediction state, also known as the time update, is made up of two steps: voltage prediction and prior error covariance. The voltage prediction is obtained by Eq. (12), and the prior error covariance is calculated based on Eq. (13).

$$\hat{V}_k^- = \hat{V}_{k-1} + M \frac{\Delta P_{pv,k-1}}{\Delta V_{pv,k-1}} \quad (12)$$

$$P_k^- = P_{k-1} + Q \quad (13)$$

where \hat{V}_k^- is the predicted V_{mpp} at k^{th} iterations, \hat{V}_{k-1} is the updated estimate of the V_{mpp} in $(k-1)^{\text{th}}$ iterations, $\Delta P_{pv,k-1}/\Delta V_{pv,k-1}$ is the instantaneous

power slope at $(k-1)^{\text{th}}$ iterations. M is the scaling factor. The scaling factor in this system is 0.5, which is obtained through trial and error. P_k^- is the a priori error covariance in k^{th} iterations, P_{k-1} is the posteriori error covariance in $(k-1)^{\text{th}}$ iterations, and Q is the process noise covariance. The value of Q in this system is 0.01.

The instantaneous power slope at $(k-1)^{\text{th}}$ iteration $k-1$ is calculated according to Eq. (14). The P-V curve in Fig. 3 shows that the power slope is positive when the PV voltage is less than V_{mpp} . The power slope is zero when the PV voltage is V_{mpp} . The power slope is negative when the PV voltage is greater than V_{mpp} .

$$\frac{\Delta P_{pv,k-1}}{\Delta V_{pv,k-1}} = \frac{P_{pv,k-1} - P_{pv,k-2}}{V_{pv,k-1} - V_{pv,k-2}} \quad (14)$$

The step after the prediction state is a measurement update or is called the correction state. The measurement update corrects the predicted value during the prediction state step. The measurement update has three equations, namely, calculating the Kalman gain (K_k), updating the estimated voltage (\hat{V}_k) and updating the error covariance (P_k). The Kalman gain was calculated according to Eq. (15).

$$K_k = P_k^- (P_k^- + R)^{-1} \quad (15)$$

The measurement noise covariance (R) represents the noise distribution at the measurement input given by the sensor. In this system, the value of R is 0.01. The updated estimate of the PV voltage at the MPP is formulated with Eq. (16), where $V_{pv,k}$ is the PV voltage at k^{th} iterations.

$$\hat{V}_k = \hat{V}_k^- + K_k \times (V_{pv,k} - \hat{V}_k^-) \quad (16)$$

The update error covariance P_k is obtained based on Eq. (17).

$$P_k = (1 - K_k) \times P_k^- \quad (17)$$

In the next iteration, \hat{V}_k becomes \hat{V}_{k-1} and P_k becomes P_{k-1} . \hat{V}_k is used as a setpoint for the MPP tracking control.

3.2 Design of fuzzy logic controller

The fuzzy logic controller (FLC) controls the DC boost converter so that the PV output power reaches the MPP. The FLC inputs are the PV voltage error (VE) and the PV voltage error change (ΔVE). The PV voltage error is the difference between the estimated PV voltage from the Kalman filter and the actual PV

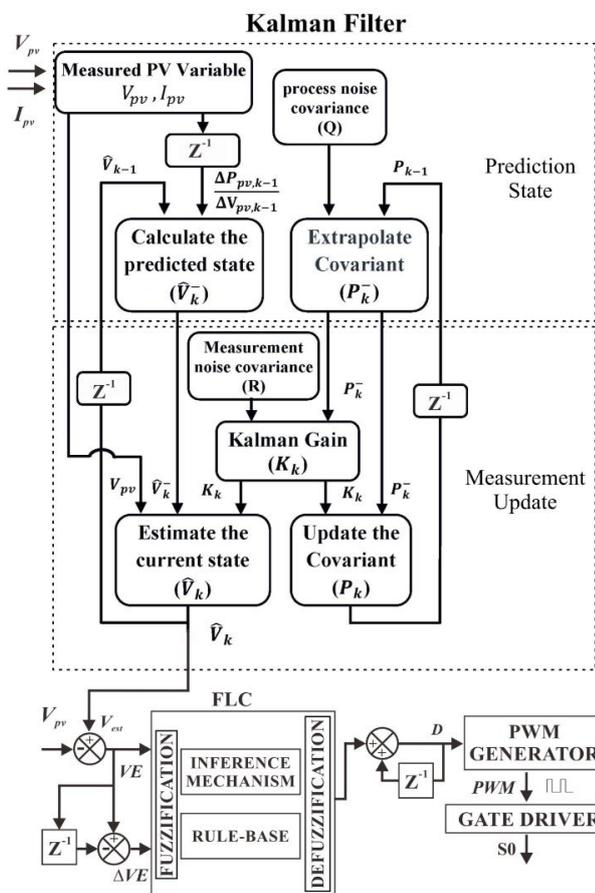


Figure. 5 Functional diagram of the HKF algorithm

voltage. The FLC output is the control signal for the DC boost converter. The position of the FLC in the MPPT system architecture is shown in Fig. 5. Fuzzy control uses linguistic variables instead of mathematical models of dynamic systems [25].

The FLC in this system uses the Mamdani method, which is often known as the max-min method. There are three stages for output control: fuzzification, inference mechanism, and defuzzification [27, 28]. Fuzzification converts crisp input values into fuzzy sets. The inference mechanism makes decision-making from the fuzzy input set based on the designed logic rules. The results of the inference mechanism were converted into sharp outputs through the defuzzification process.

The voltage error (VE) and delta voltage error (ΔVE) as FLC input variables are transformed into input membership functions, as shown in Fig. 6(a) and 6(b). The input membership function of VE is divided into five linguistic labels, including high negative error (HNE), low negative error (LNE), zero error (ZE), high positive error (HPE), and low positive error (LPE). The input membership function

of ΔVE is divided into five linguistic labels: delta high negative error (DHNE), delta low negative error (DLNE), delta zero error (DZE), delta low positive error (DLPE), and delta high positive error (DHPE).

The FLC output is a control signal represented as a step size D . The magnitude of D results from the sum of the previous D values with the FLC output. The FLC output membership function is shown in Fig. 6(c). The FLC output function is divided into five linguistic labels, which include the high negative output (HNO), low negative output (LNO), zero output (ZO), low positive output (LPO), and high positive output (HPO). The logical rules built into the inference mechanism are based on human experience embodied through language variables and rule-based. The FLC rule in the proposed method uses 25 rule bases represented in a symmetrical form, as shown in Table 4. There are several defuzzification methods in the Mamdani method, and this system uses the centroid method. The crisps output (z) is obtained by taking the center point of the fuzzy area based on Eq. (18).

$$z = \frac{\sum_{i=1}^n z_i \mu(z_i)}{\sum_{i=1}^n \mu(z_i)} \quad (18)$$

where z is the center point of the fuzzy area, z_i is the sample element, $\mu(z_i)$ is the membership function, and n represents the number of elements in the sample.

4. Simulation and experimental

4.1 Simulation setup

The SPVPIS model was simulated using MATLAB/Simulink. This system consists of a PV model, DC boost converter model, MPPT controller model, BLDC motor model, centrifugal water pump model, irrigation network model, and irrigation sector controller. The HKF method as an MPPT control strategy has input from the PV output voltage and current sensor. The values of the Q and R parameters of the Kalman filter are 0.01 and 0.01, respectively. The HKF output is a control signal in the form of PWM to control the boost converter so that

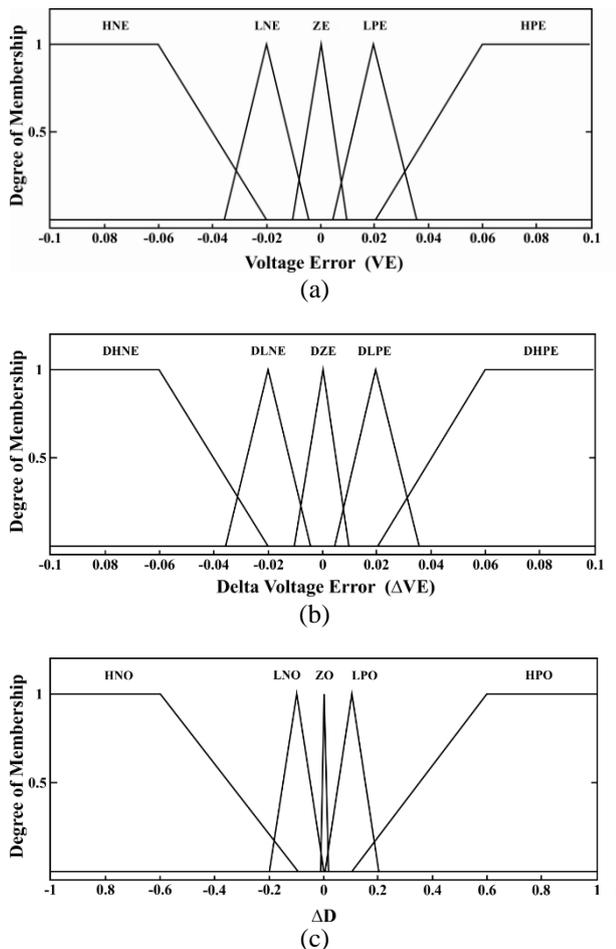


Figure. 6 Fuzzy membership function of: (a) voltage error, (b) delta voltage error, and (c) output FLC

Table 4. Fuzzy rule-based

$VE \backslash \Delta VE$	HNE	LNE	ZE	LPE	HPE
DHNE	HNO	HNO	LNO	HPO	HPO
DLNE	HNO	LNO	LNO	LPO	HPO
DZE	LNO	LNO	ZO	LPO	LPO
DLPE	HNO	LNO	LPO	LPO	HPO
DHPE	HNO	HNO	LPO	HPO	HPO

the PV output power is always at the MPP.

The pressurized irrigation system (PIS) model resulted from the integration of several models, namely BLDC motors, centrifugal water pumps, irrigation networks, and irrigation sector controllers. The irrigation network was divided into ten sectors with a capacity of 10 W in each sector. The number of active sectors increased if the PV output power increased by more than 10 W, and vice versa. The irrigation sector is regulated by a multi-sector controller based on the PV output power through activation of the solenoid valve. The match between the PV output power and irrigation capacity will result in an IOP closer to the setpoint and more stable.

SPVPIS model testing has been carried out to determine the characteristics and performance of the proposed method. The observed MPPT variables include power, voltage, and current at the PV output. The observed PIS variables include motor speed (N) in the RPM, motor torque (T) in Nm, stator back EMF in volts and, IOP in psi. Perturb and Observe (P&O) is another method used for comparison. The P&O method was applied to the same SPVPIS to determine the advantages of the HKF method over other methods.

The test was performed by changing the PV irradiation to several patterns. This study has three test patterns: a unit step pattern and two natural data patterns. The unit step pattern was used to determine the response speed and steady-state of the MPPT system. Natural data patterns were used to assess the ability of the MPPT system to adapt to natural changes during irradiation. The data pattern was obtained from daily solar radiation recordings on the Institut Teknologi Sepuluh Nopember (ITS), Surabaya, Indonesia. The ITS PV station has a 16 kW rooftop photovoltaic power plant installed at coordinates $7^{\circ}16'52.4892''S$, $112^{\circ}47'50.838''E$. The irradiation pattern used in this test was recorded on June 13, 2021, and July 17, 2021.

The unit step test pattern was shown in Fig. 7. The irradiation pattern started from 300 W/m^2 irradiation for 200 ms, then changed to 400 W/m^2 for 200 ms and 500 W/m^2 for 200 ms. This test with tiered irradiation

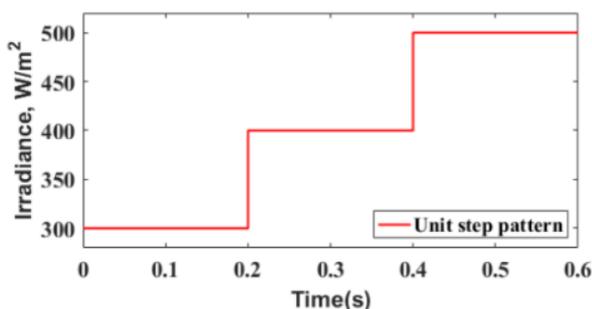


Figure. 7 Unit step pattern for performance test

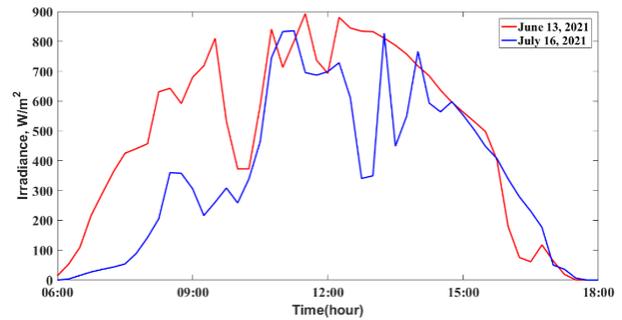


Figure. 8 Daily irradiation at the ITS PV panel station on June 13, 2021, and July 17, 2021

changes is to determine the MPPT response at each different irradiation level. The simulation model was tested with two natural data patterns. The natural data pattern corresponds to the daily solar radiation recorded by the ITS PV panel station. Fig. 8 is 2 data on daily solar irradiance recorded on June 13, 2021, and July 17, 2021. The irradiation value in these data is very volatile because the weather changes rapidly. A sharp decrease in irradiation due to cloud shadows covering the PV panels. This pattern is good enough to test the ability of the MPPT method because the irradiation changes are dynamic. The pattern used to test the simulation has the same irradiation magnitude as the daily irradiation pattern but with a downscaling duration.

4.2 Simulation performance

The test results of the SPVPIS simulation using the unit step pattern are shown in Fig. 9. The MPPT response is shown in Fig. 9(a), while the IOP response of the irrigation network is shown in Fig. 9(b). It can be seen that the HKF method can track the MPP quickly and has small steady-state oscillations. Although the P&O method was also successful in tracking MPP, it had larger oscillations than the HKF method. The magnification of the graphic display of the MPPT transition response when the irradiation changes are shown in Fig. 10. The response of the system from the beginning to reach MPP of 30.19 W at an irradiation of 300 W/m^2 is shown in Fig. 10(a). Fig. 10(b) is the transition response of the system due to irradiation from 300 W/m^2 to 400 W/m^2 . Fig. 10(c) is the transition response from irradiation of 400 W/m^2 to 500 W/m^2 . The MPP value of PV panels at 400 W/m^2 irradiation is 40.47 W, and at 500 W/m^2 irradiation is 50.67 W. The rise time and steady-state oscillation values for each transition are summarized in Table 5. The HKF method has an average rise time of 1.9 ms and an average steady-state oscillation amplitude of 0.65 W with a frequency of 683.54 Hz. The P&O method has an average rise time of 24.5 ms and an average

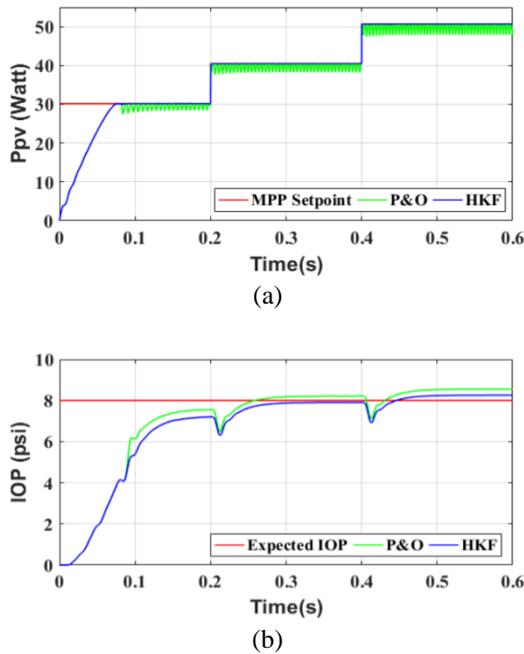


Figure 9 SPVPIS simulation test results with unit step pattern, (a) the MPPT response and (b) the IOP response

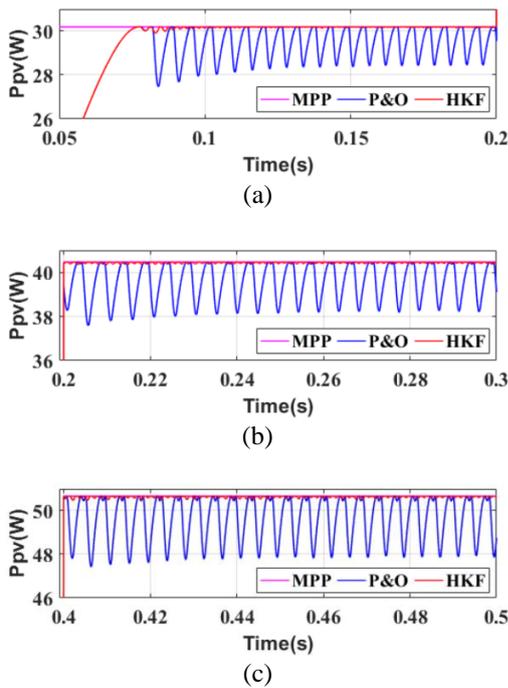


Figure 10 Magnification of the MPPT transition response, (a) 0 W/m² to 300W/m², (b) 300W/m² to 400W/m², (c) 400W/m² to 500W/m²

Table 5. Comparison of the HKF and P&O method test results

Irradiance (W/m ²)	Rise time (ms)		Oscillations (W)	
	HKF	P&O	HKF	P&O
300	93	110	0.03	1.75
400	1.7	21	0.06	2.12
500	2.1	28	0.07	2.75

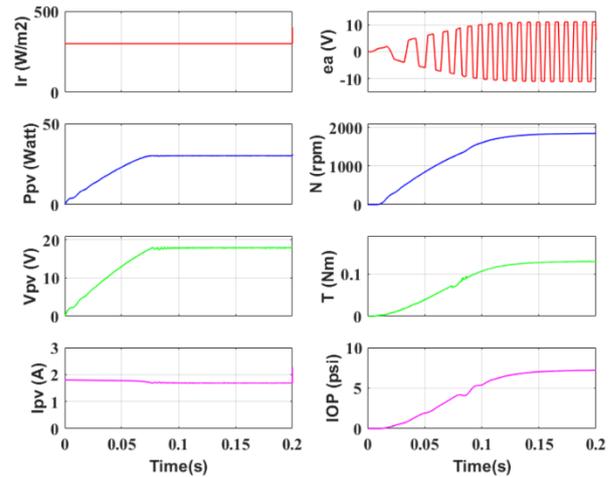


Figure 11 Responses of PIS at the beginning simulation

steady-state oscillation amplitude of 2.4 W with a frequency of 211.27 Hz. At the beginning of the simulation, the rise time was much longer than that after passing the first steady-state. This is caused by the BLDC motor starting and initial charging of the capacitor in the boost converter. Starting on a BLDC motor requires an inrush current of 3-5 times the nominal current.

Compared to the P&O method, the HKF method has a shorter rise time and steady-state oscillation. The fast response and low steady-state oscillation in the HKF method are due to the ability of the Kalman filter to estimate the MPP and the ability of the FLC to regulate the duty cycle step size of the boost converter. The accuracy of this FLC control is strongly influenced by the accuracy of the membership function design based on the control logic and the characteristics of the boost converter. The conventional P&O method has a fixed duty cycle step size, whereas the HKF method has a variable duty cycle step size. The duty cycle step size is based on the difference between the actual PV output voltage and estimated V_{mpp} . Therefore, if the V_{mpp} estimation by the Kalman filter is inaccurate, FLC control will be inaccurate.

The characteristics of the IOP response to changes in irradiation are shown in Fig. 8(b). It can be seen that the IOP on the PIS can reach the expected value even though the PV output power changes. At the beginning of the simulation, the IOP rise time was longer than that after passing the first steady-state because of the pump starting process. The process variables for the MPPT and PIS at the beginning of the simulation are shown in Fig. 11. It can be seen that the PV output current when the BLDC motor starts is 1.8 A. This value is the maximum output current of the 100Wp PV panel when the irradiation is 300 W/m². The speed and torque of the BLDC

motor start to be constant when the MPPT reaches its optimum power, resulting in a constant IOP. The residual pressure due to the reduced number of active sectors resulted in a temporary spike in IOP. The momentary decline in IOP results from an increase in the number of active sectors.

The simulation test results using natural irradiation pattern data recorded on June 13, 2021, are shown in Fig. 12(a) and 12(b). The test results with natural irradiation pattern data recorded on July 16, 2021, are shown in Fig. 13(a) and 13(b).

The system response to the two test patterns shows that the HKF and P&O methods can track MPP values at all irradiation levels even though the irradiation changes dynamically. However, the HKF method is superior to the conventional P&O method because it has a smaller steady-state oscillation amplitude. The largest oscillation amplitudes of the HKF method tested with irradiation patterns on June 13, 2021, and July 17, 2021, were 0.33 W and 0.36 W, respectively, while the P&O method was 5.06 W and 5.15 W, respectively. The PIS response shows

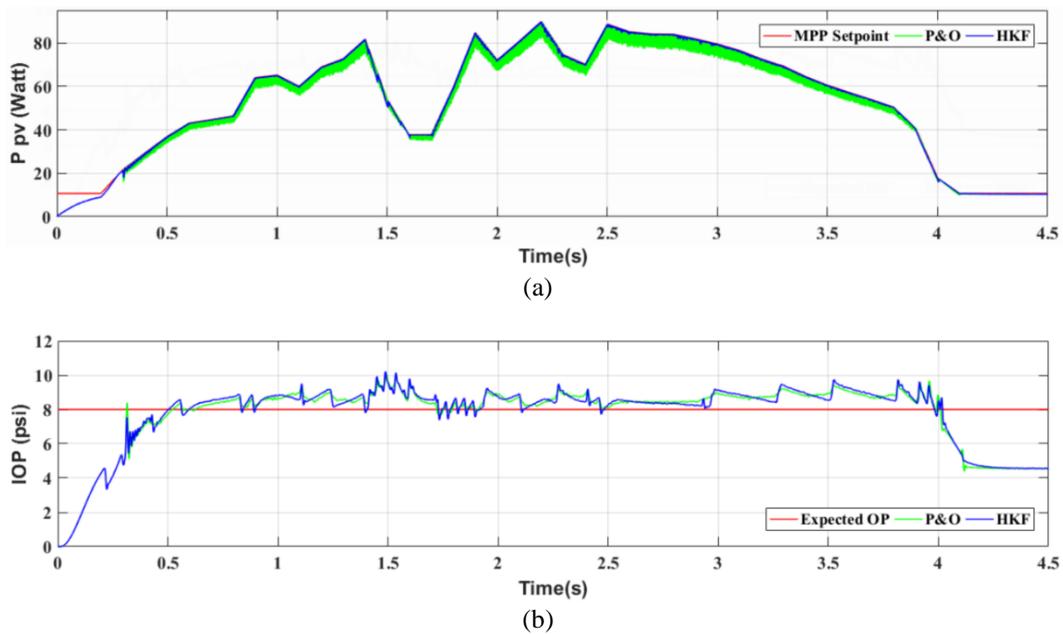


Figure. 12 Simulation test results using natural irradiation patterns recorded by ITS PV station on June 13, 2021, (a) MPPT control response and (b) irrigation network response

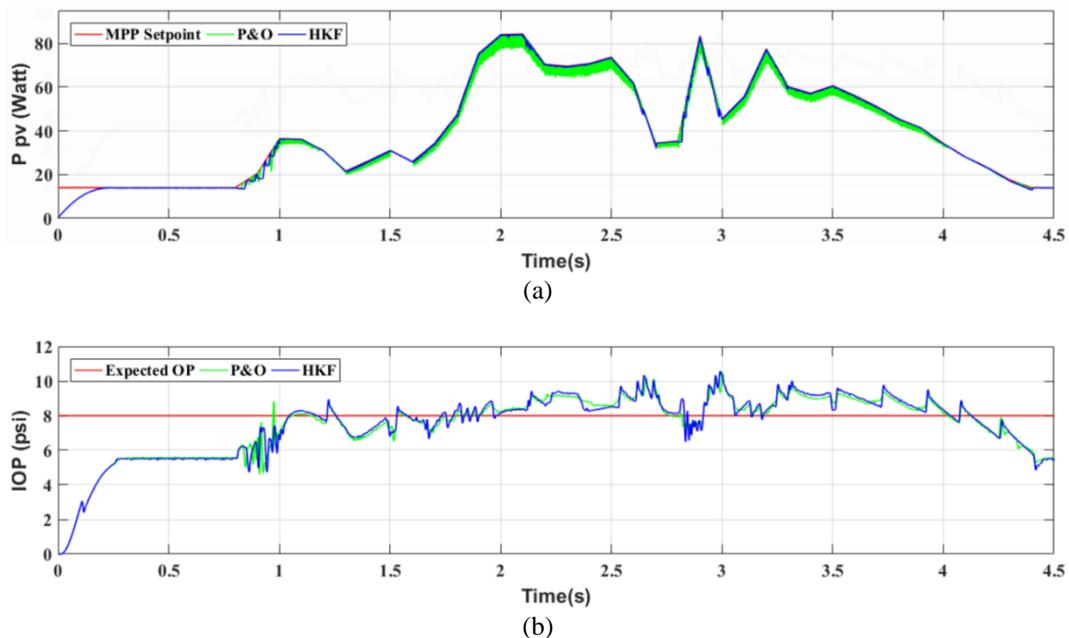


Figure. 13 Simulation test results using natural irradiation patterns recorded by ITS PV station on July 17, 2021: (a) MPPT control response and (b) irrigation network response

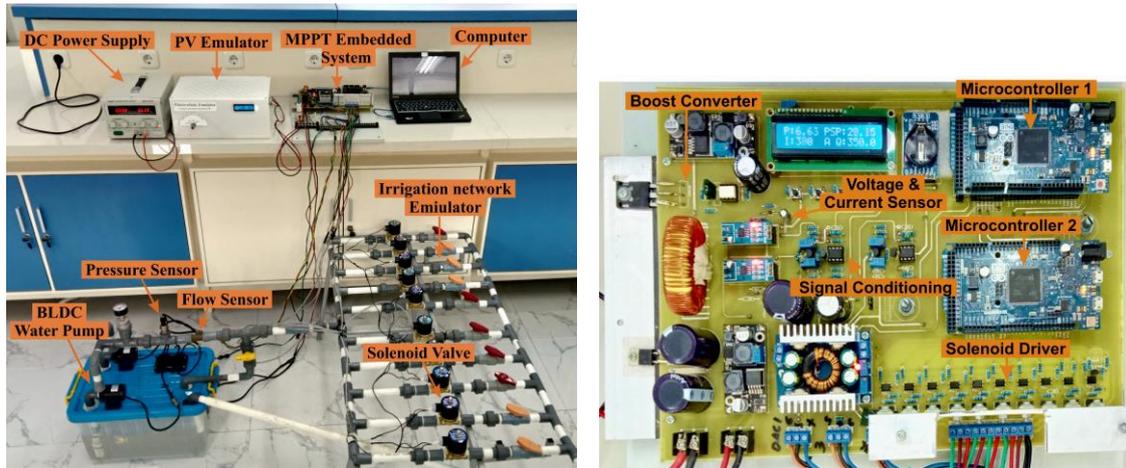


Figure. 14 SPVPIS prototype used to validate the proposed method: (a) Photo of SPVPIS prototype and (b) Embedded system

IOP fluctuating 0-2 psi around the planned value of 8 psi. This fluctuation results from the irrigation sector controller using the on/off method. However, the concept of regulating IOP by controlling irrigation capacity according to the PV output power has succeeded in making IOP more stable.

4.3 Experimental setup

The performance of the proposed MPPT method was validated using the SPVPIS prototype. The prototype consists of an MPPT module, an irrigation control module, and a pressurized irrigation network. The pressurized irrigation emulator consists of a BLDC pump, water reservoir, pressure sensor, flow sensor, solenoid valve, stop valve, and parallel pipe. The integration between the embedded systems, PV panels, and pressurized irrigation networks into the SPVPIS is shown in Fig. 14(a).

The MPPT hardware and irrigation control modules were built into an embedded system, as shown in Fig. 14(b). The MPPT system consists of an ARM-32 microcontroller, boost converter, Hall effect-based current sensor, voltage sensor, and signal conditioner. The irrigation control system includes an ARM-32 microcontroller, signal conditioner, water pressure sensor, water flow sensor, and solenoid valve driver. The output signal from the voltage, current, and water pressure sensors is amplified by a conditioning signal and then converted to digital data using a 10-bit Analog to Digital converter (ADC) in the microcontroller. Data from the ADC filtered using a moving average filter to reduce the noise. The communication between the two microcontrollers uses an asynchronous serial.

The HKF method algorithm implemented in microcontroller 1 has a program flow chart, as shown

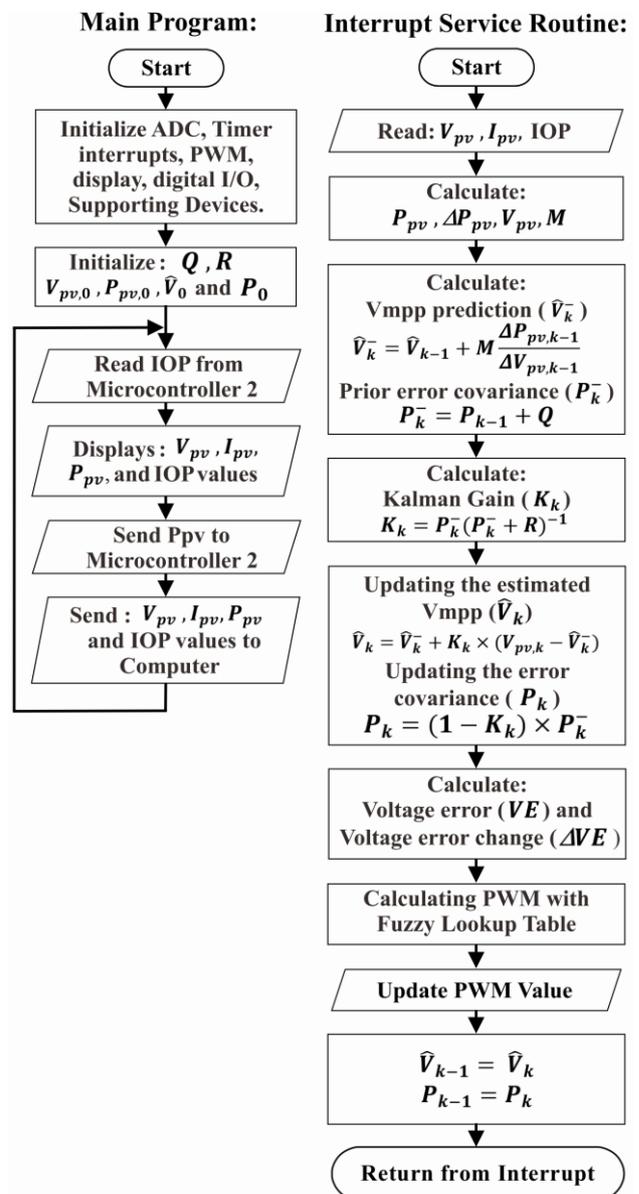


Figure. 15 Flow chart of the HKF method implemented in the microcontroller

in Fig. 15. The program flow consists of 2 parts: the main program and the interrupt service routine (ISR).

The main program only reads the IOP value from microcontroller 2, sends the actual PV power value, displays the PV output variable and IOP to the local display, sends this SPVPIS variable measurement data to the computer, and waits for the timer interrupt. The program, which includes PV variable reading, V_{mpp} estimation with Kalman filter, and FLC algorithm with a lookup table (LUT), is carried out at ISR. The data sampling process is carried out in the interrupt timer resulting in a stable sampling period.

The SPVPIS hardware was tested using a PV emulator. The PV emulator is a nonlinear power supply capable of producing a current-voltage characteristic similar to a PV panel [29-31]. Testing the MPPT method using a PV emulator is more accessible and scalable. The prototype test was carried out by changing the PV emulator irradiation value with a unit step pattern from 320W/m^2 to 527W/m^2 and from 527W/m^2 to 683W/m^2 .

4.4 Experiment Performance

Measurements of voltage and current at the PV output and IOP carried out by the microcontroller have average errors of 0.6%, 2.5%, and 1%, respectively. Testing the prototype for 55 s with a rapidly changing irradiation pattern results in a response, as shown in Fig. 16. For comparison, the graph also includes the results of testing the simulation model with the same

treatment. The HKF-based MPPT response is shown in Fig. 16(a). It can be seen that the application of the HKF method on the prototype can track and condition the PV output power to reach the MPP. The system rise time in tracking the MPP when the irradiance is changed from 320W/m^2 to 527W/m^2 or from 527W/m^2 to 683W/m^2 is 1.02 s. The rise time value of the prototype test results was greater than that of the simulation results. Some factors that cause a larger prototype rising time are less than ideal component characteristics, low computational speed of the microcontroller, the time lag in the moving average filter, and relatively slow sampling time. The sampling time on this microcontroller was $1\mu\text{s}$. The prototype response is faster when using a microcontroller with a higher speed.

The response of the irrigation network to the prototype is shown in Fig. 16(b). Although the solar irradiation changed, the IOP variable was relatively stable around the expected value of 8 psi. There is a slight decrease in IOP when the PV power changes by more than 30 W owing to changes in the number of active irrigation sectors. The IOP ripple in the simulation is higher and more numerous than in the experiment because the water pressure sensor is less sensitive to small and sudden pressure changes and the influence of the moving average filter in the microcontroller algorithm.

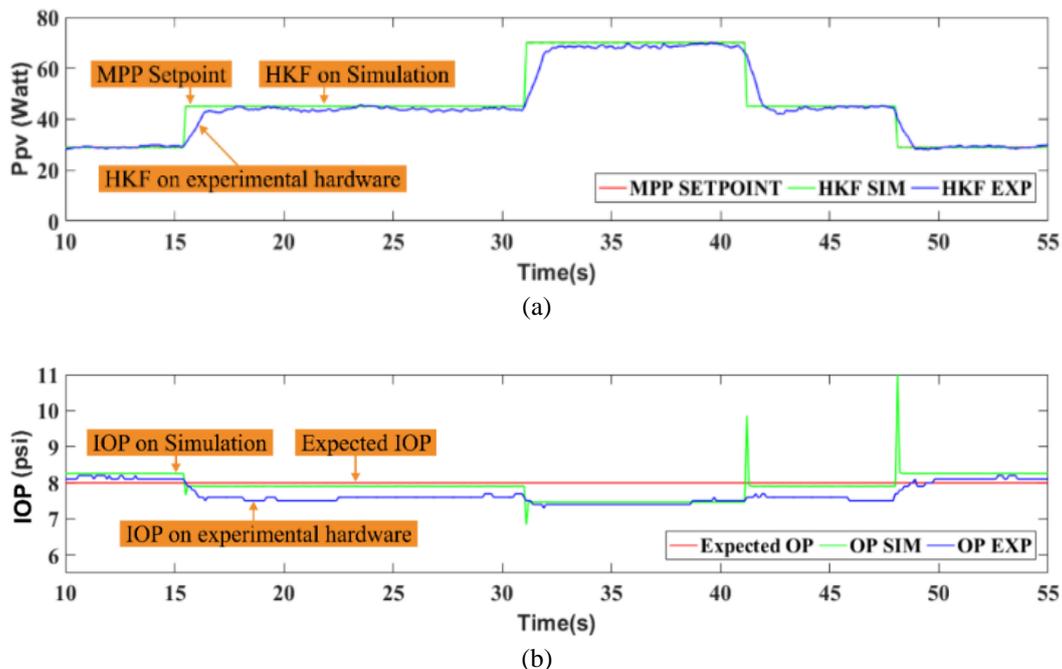


Figure. 16 Experimental test results with variations in irradiation: (a) MPPT control response and (b) irrigation network response

Table 6. Comparison of MPPT and irrigation system performance

Performance	PV panel	MPPT Method	DC Converter	Motor-pump	Irrigation type	MPPT transient responses	MPPT steady-state oscillation	IOP response
Ref [11]	Yes	INC	No	BLDC	Surface	Middle	Middle	No
Ref [12]	Yes	INC	Cuk	BLDC	Surface	Middle	Middle	No
Ref [13]	Yes	INC	Landsman	BLDC	Surface	Middle	Middle	No
Ref [14]	Yes	INC	Zeta	BLDC	Surface	Middle	Middle	No
Ref [15]	Yes	FLC	Boost	Induction	Surface	Middle	Middle	No
Ref [16]	No	No	No	DC Brush	Pressurized	No	No	Stable
Ref [17]	Yes	No description	No description	Induction	Pressurized	No description	No description	Stable
Proposed	Yes	HKF	Boost	BLDC	Pressurized	low	low	Stable

4.5 Performance comparison Of MPPT and irrigation methods

The comparison of the performance of the proposed system, namely SPVPIS based on the HKF-MPPT method, against other irrigation systems in the literature is shown in Table 6. The comparison includes PV as an energy source, the MPPT method used, the type of DC converter, the kind of pump driving motor, the type of irrigation, MPPT transient response, and MPPT steady-state, and IOP response. Other irrigation systems in the literature have not yet integrated the optimization of PV output power with irrigation capacity. Some irrigations that optimize irrigation capacity have not been synchronized with energy sources. This synchronization is needed to reduce the number of PV panels. MPPT with the HKF method has a much better performance than the system in the literature. MPPT HKF method has a faster transient response and smaller power oscillations in MPP.

5. Conclusions

The proposed HKF method was applied to the SPVPIS without energy storage. The system was simulated using MATLAB/Simulink and implemented in a laboratory-scale prototype. The simulation test results using the unit step pattern show that the system has an average rise time of 1.9 ms and an average steady-state oscillation amplitude of 0.65 W with a frequency of 683.54 Hz. The simulation test results on the SPVPIS model using natural irradiation patterns show that the HKF method can achieve MPP with a maximum steady-state oscillation of 0.36 W. The performance of the HKF method is much better than that of the conventional P&O method because it has a shorter rise time and steady-state oscillation. The prototype test results using the unit step pattern showed that the HKF method achieved MPP at all

irradiation levels with a rise time of 1.02 s. The fast response and low steady-state oscillation in the HKF method are due to the ability of the Kalman filter to estimate the V_{mpp} and the ability of the FLC to regulate the duty cycle step size of the boost converter.

The success of the HKF method in optimizing PV output power results in better irrigation performance and precision. The simulation and prototype test results showed that the IOP in the PIS was maintained around the expected value. However, the PV output power and the number of irrigation sectors have changed.

Conflicts of Interest

The authors declare no conflict of interest.

Author Contributions

In this research article author contributions are as follows: “Conceptualization and methodology, Suwito Suwito, and Mochamad Ashari; software, Suwito Suwito; validation, Suwito Suwito, Mochamad Ashari and Muhammad Rivai; formal analysis, Suwito Suwito, Mochamad Ashari and Muhammad Rivai; investigation, Suwito Suwito; resources, Suwito Suwito; data curation, Suwito Suwito; writing—original draft preparation, Suwito Suwito; writing—review and editing, Suwito Suwito, Mochamad Ashari, Muhammad Rivai, and M. Anis Mustaghfirin; visualization, Suwito Suwito; supervision, Mochamad Ashari, Muhammad Rivai, and M. Anis Mustaghfirin”.

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